

# Research Report

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# Overview

- ❑ **Lecture on Numerical Simulation on Coupled Field Problems**
  - ❑ Fluid-Structure-Acoustics
  - ❑ Piezoelectricity
  - ❑ Magnetomechanics
  - ❑ MHD and Porous Media (Marco Discacciati)
- ❑ **Workshop on** (together with B. Kaltenbacher)  
***Direct and Inverse Problems in Piezoelectricity***
- ❑ **Computation of thin (flat) structures (D. Braess)**
  - Mechanical structures
  - Piezoelectric structures
- ❑ **Perfectly matched layers (PMLs) (J. Schöberl)**
  - Splitting approach
  - Analytic continuation approach
  - Time domain approach
- ❑ **Further cooperations**

# Computation of thin (flat) Structures (I)

## □ Reissner-Mindlin-formulation

$$\Pi(\vartheta, \omega) = \frac{1}{2} \int_{\Omega} \varepsilon(\vartheta) \mathbf{D}_{\text{plate}} \varepsilon(\vartheta) d\Omega + \frac{1}{t^2} \int_{\Omega} |\nabla \omega - \vartheta|^2 d\Omega$$

## □ Appropriate mixed formulation

$$\gamma := t^{-2}(\nabla \omega - \vartheta) \quad \text{shear term}$$

$$a(\vartheta, \psi) + \frac{1}{h^2}(\nabla \omega - \vartheta, \nabla v - \psi) + (\nabla v - \psi, \gamma) = (f, v)$$

$$(\nabla \omega - \vartheta, \eta) - t^2(\gamma, \eta) = 0$$

# Computation of thin (flat) Structures (II)

- Instead of mixed formulation, solve

$$\begin{aligned} a(\vartheta_h, \psi) &+ k\alpha(\nabla \omega_h - \vartheta_h, \nabla v - \psi) \\ &+ k^2(t^{-2} - \alpha)(\pi_h[\nabla \omega_h - \vartheta_h], \pi_h[\nabla v - \psi]) \\ &= (f, v) \end{aligned}$$

Computes mean value  
over each element

- Arnold & Brezzi

$$\alpha = \frac{1}{t^2} - \alpha > 0, \quad \alpha = \text{const.}$$

- Chapell & Stenberg

$$\alpha = \frac{\mu}{t^2 + h^2}, \quad \mu = \text{const.}$$

# Computation of thin (flat) Structures (III)

## □ 3D formulation

$$\int_{\Omega} \varepsilon_{13}(u)^2 d\Omega \approx t \quad \int_{\Omega} \varepsilon_{11}(u)^2 d\Omega \approx t^3$$

$$\mathbf{D} := \mathbf{D}_b + \mathbf{D}_s$$

$$\mathbf{D}_b = \begin{pmatrix} c_{11} & c_{12} & c_{13} & 0 & 0 & 0 \\ c_{12} & c_{22} & c_{23} & 0 & 0 & 0 \\ c_{13} & c_{23} & c_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & \alpha * c_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & \alpha * c_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & \alpha * c_6 \end{pmatrix} \quad \mathbf{D}_s = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \beta * c_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & \beta * c_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & \beta * c_6 \end{pmatrix}$$

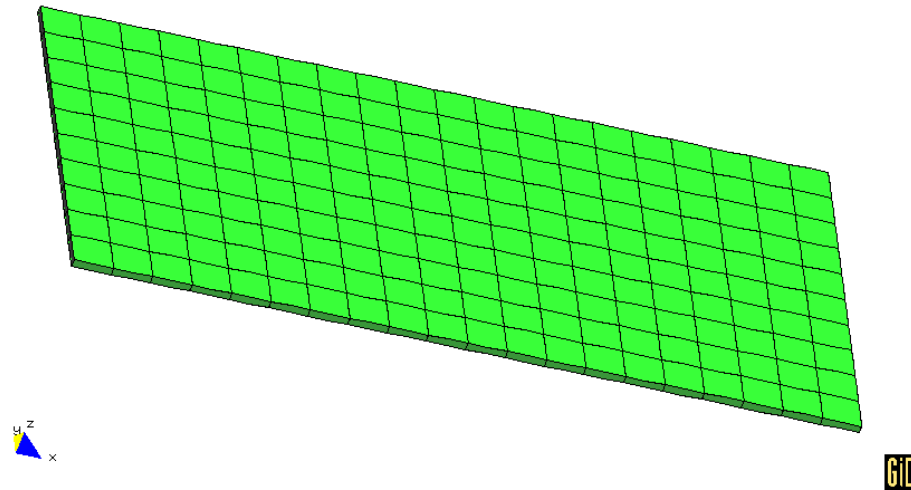
$$\alpha = \frac{t^2}{h^2 + t^2}$$

$$\beta = \frac{h^2}{h^2 + t^2}$$

$$\mathbf{k}^e = \underbrace{\int_{\Omega^e} \mathcal{B} \mathbf{D}_b \mathcal{B} d\Omega}_{\text{standard integration}} + \underbrace{\int_{\Omega^e} \mathcal{B} \mathbf{D}_s \mathcal{B} d\Omega}_{\text{reduced integration}}$$

# Computation of thin (flat) Structures (IV)

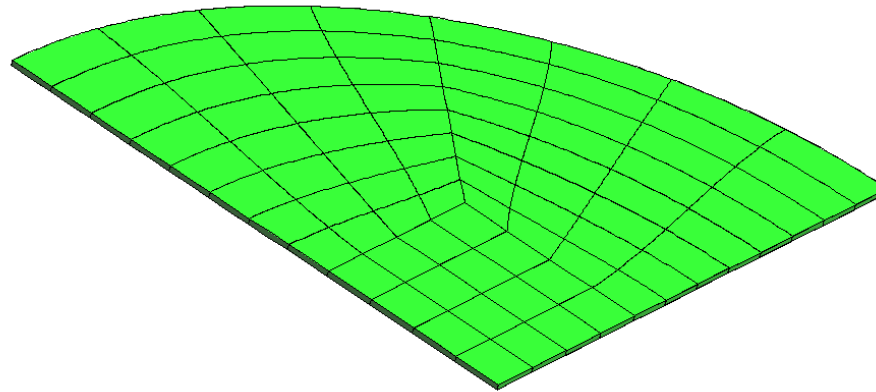
□ Plate:  $2a \times 2b$ ,  $a=20\text{mm}$ ,  $b=10\text{mm}$ ,  $t=0.2\text{mm}$



$h/t$	lin	lin-SRI	lin-BK	quad	quad-BK	Kirchhoff
25	$0.072 \mu\text{m}$	$9.531 \mu\text{m}$	$7.49 \mu\text{m}$	$9.17 \mu\text{m}$	$12.74 \mu\text{m}$	$13.47 \mu\text{m}$
10	$0.426 \mu\text{m}$	$11.70 \mu\text{m}$	$9.23 \mu\text{m}$	$13.32 \mu\text{m}$	$13.77 \mu\text{m}$	$13.47 \mu\text{m}$
5	$1.528 \mu\text{m}$	$12.04 \mu\text{m}$	$9.43 \mu\text{m}$	$13.75 \mu\text{m}$	$13.83 \mu\text{m}$	$13.47 \mu\text{m}$
2	$5.586 \mu\text{m}$	$12.12 \mu\text{m}$	$9.80 \mu\text{m}$	$13.84 \mu\text{m}$	$13.84 \mu\text{m}$	$13.47 \mu\text{m}$
1	$9.003 \mu\text{m}$	$12.13 \mu\text{m}$	$9.002 \mu\text{m}$	$13.84 \mu\text{m}$	$13.84 \mu\text{m}$	$13.47 \mu\text{m}$

# Computation of thin (flat) Structures (V)

□ Plate:  $R=,20\text{mm}$   $t=0.2\text{mm}$

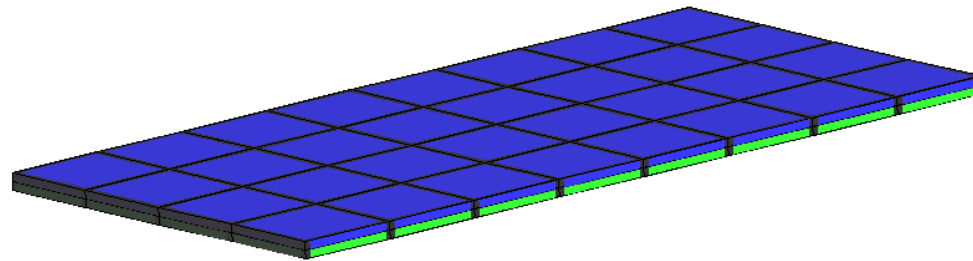


GTU

$h/t$	lin	lin-SRI	lin-BK	quad	quad-BK	Kirchhoff
16.25	$1.16 \mu\text{m}$	$99.11 \mu\text{m}$	$72.92 \mu\text{m}$	$99.08 \mu\text{m}$	$105.06 \mu\text{m}$	$108.62 \mu\text{m}$
8.125	$4.39 \mu\text{m}$	$103.59 \mu\text{m}$	$75.49 \mu\text{m}$	$106.87 \mu\text{m}$	$108.27 \mu\text{m}$	$108.62 \mu\text{m}$
4	$15.18 \mu\text{m}$	$105.00 \mu\text{m}$	$76.58 \mu\text{m}$	$108.40 \mu\text{m}$	$108.65 \mu\text{m}$	$108.62 \mu\text{m}$
2	$39.89 \mu\text{m}$	$105.55 \mu\text{m}$	$78.87 \mu\text{m}$	$108.70 \mu\text{m}$	$108.73 \mu\text{m}$	$108.62 \mu\text{m}$
1	$67.47 \mu\text{m}$	$105.85 \mu\text{m}$	$83.78 \mu\text{m}$	$108.78 \mu\text{m}$	$108.79 \mu\text{m}$	$108.62 \mu\text{m}$

# Computation of thin (flat) Structures (VI)

- Plate with piezoelectric layer:  $a=20\text{mm}$ ,  $b=10\text{mm}$ ,  $t_{1,2}=0.1\text{mm}$

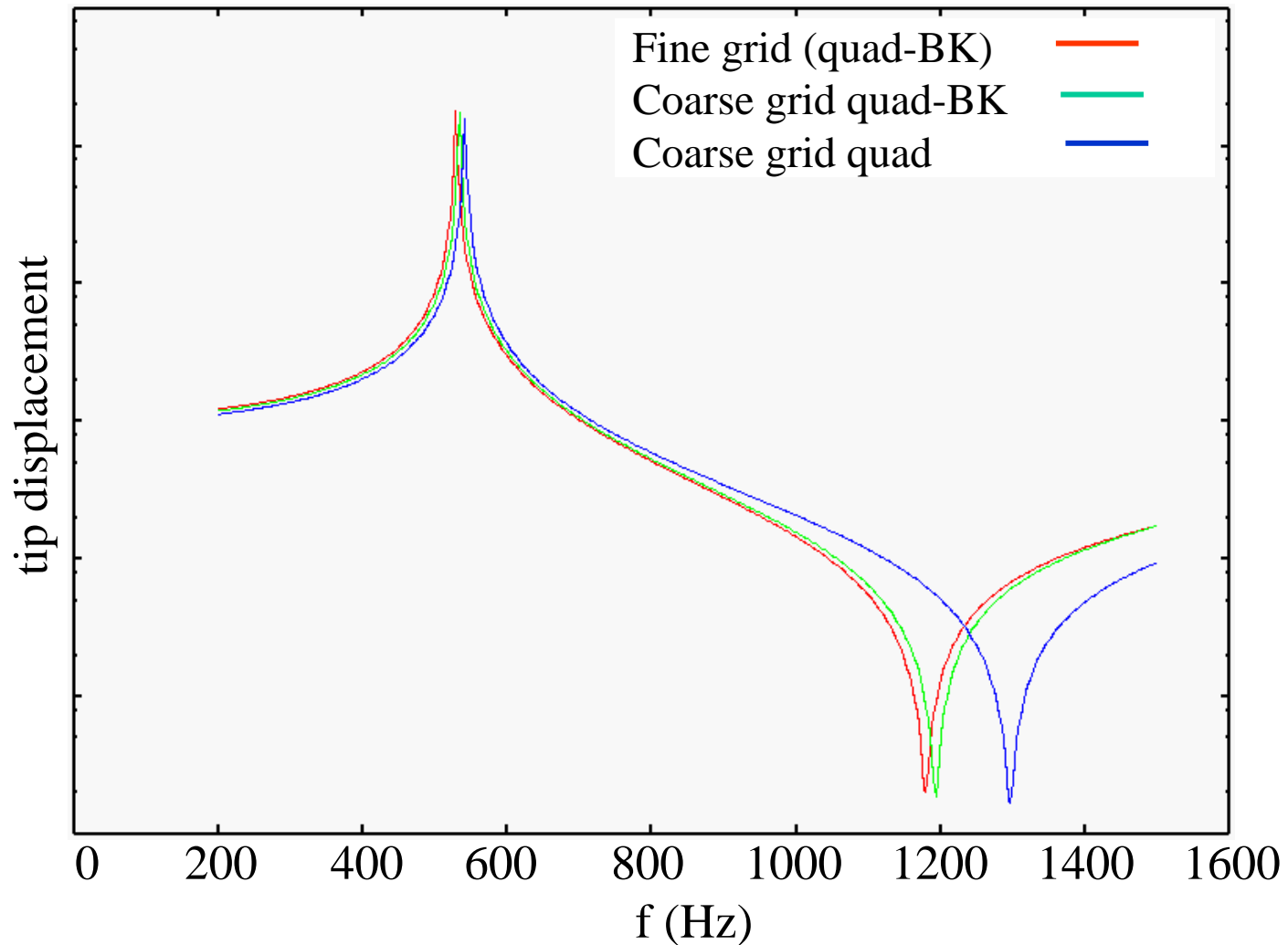


$h/t$	lin	lin-SRI	lin-BK	quad	quad-BK
50	$0.081 \mu\text{m}$	$12.30 \mu\text{m}$	$11.00 \mu\text{m}$	$11.32 \mu\text{m}$	$11.75 \mu\text{m}$
25	$0.32 \mu\text{m}$	$12.67 \mu\text{m}$	$11.28 \mu\text{m}$	$11.57 \mu\text{m}$	$11.70 \mu\text{m}$
12.5	$1.18 \mu\text{m}$	$12.77 \mu\text{m}$	$11.35 \mu\text{m}$	$11.65 \mu\text{m}$	$11.70 \mu\text{m}$



# Computation of thin (flat) Structures (VII)

## □ Plate with piezoelectric layer



# Perfectly Matched Layer (I)

## □ Idea of Berenger: Splitting of physical quantities

### □ PDE: linear acoustics $p' = \rho_0 c^2 \rho'$

$$\frac{\partial p'}{\partial t} = -\rho_0 c^2 \nabla \cdot \mathbf{v}' \quad \frac{\partial \mathbf{v}'}{\partial t} = -\frac{1}{\rho_0} \nabla p'$$

### □ Splitted formulation $p' = p_x + p_y + p_z$

$$\begin{aligned} \frac{\partial p_x}{\partial t} + \sigma_x p_x &= -\rho_0 c^2 \frac{\partial v_x}{\partial x} & \frac{\partial v_x}{\partial t} + \sigma_x v_x &= -\frac{1}{\rho_0} \frac{\partial p}{\partial x} \\ \frac{\partial p_y}{\partial t} + \sigma_y p_y &= -\rho_0 c^2 \frac{\partial v_y}{\partial y} & \frac{\partial v_y}{\partial t} + \sigma_y v_y &= -\frac{1}{\rho_0} \frac{\partial p}{\partial y} \\ \frac{\partial p_z}{\partial t} + \sigma_z p_z &= -\rho_0 c^2 \frac{\partial v_z}{\partial z} & \frac{\partial v_z}{\partial t} + \sigma_z v_z &= -\frac{1}{\rho_0} \frac{\partial p}{\partial z} \end{aligned}$$

# Perfectly Matched Layer (II)

## □ Analytic continuation of solution (Teixeira, Chew)

$$x_i \Rightarrow \tilde{x}_i = \int_0^{x_i} \gamma(\xi) d\xi$$
$$\gamma(x_1) = 1 + \frac{\sigma(x_i)}{j\omega}$$
$$\frac{\partial}{\partial x_i} \Rightarrow \frac{\partial}{\partial \tilde{x}_i} = \frac{1}{\gamma(x_1)} \frac{\partial}{\partial x_i}$$

## □ Acoustic PDE (Helmholtz)

$$\begin{aligned} & \gamma(x_2)\gamma(x_3) \frac{\partial}{\partial x_1} \left( \frac{1}{\gamma(x_1)} \frac{\partial p}{\partial x_1} \right) \\ & + \gamma(x_1)\gamma(x_3) \frac{\partial}{\partial x_2} \left( \frac{1}{\gamma(x_2)} \frac{\partial p}{\partial x_2} \right) \\ & + \gamma(x_1)\gamma(x_2) \frac{\partial}{\partial x_3} \left( \frac{1}{\gamma(x_3)} \frac{\partial p}{\partial x_3} \right) = \gamma(x_1)\gamma(x_2)\gamma(x_3) k^2 p \end{aligned}$$

# Perfectly Matched Layer (III)

## □ Reflection coefficient

$$R = e^{-\frac{\cos \vartheta}{c} \int_0^L \sigma(x_i) dx_i}$$

## □ Choice of damping factor ( $R \approx 10^{-3}$ )

### □ Constant

$$\sigma(x_i) = \sigma_0 \quad \sigma_0 = \frac{c \ln R}{2L \cos \vartheta}$$

### □ Quadratic distance weighting

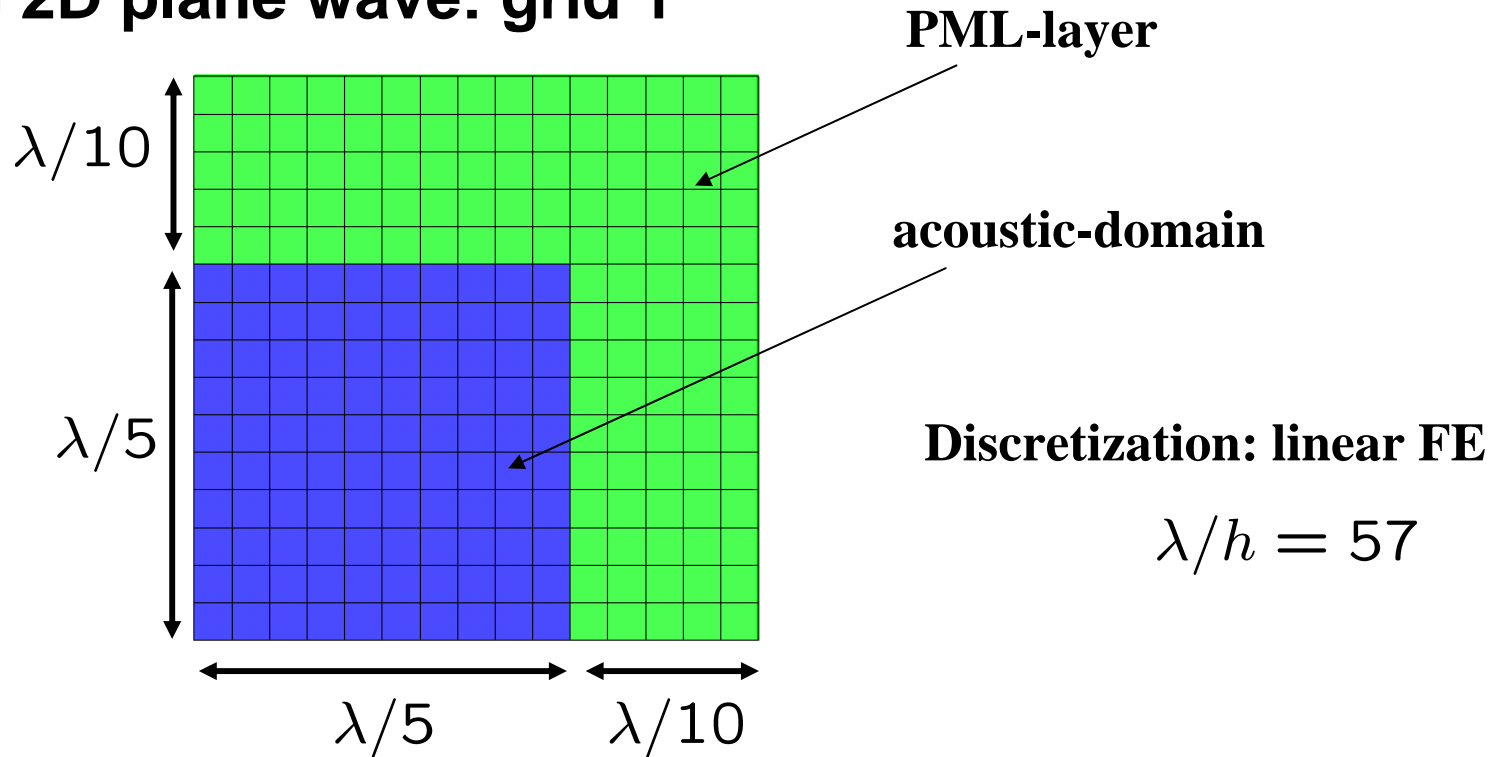
$$\sigma(x_i) = \sigma_0 \frac{x_i^2}{L^2} \quad \sigma_0 = \frac{3c \ln R}{2L \cos \vartheta}$$

### □ Inverse distance weighting

$$\sigma(x_i) = \frac{c}{L - |x_i|} \quad \int_0^L \sigma(x_i) dx_i = \infty$$

# Perfectly Matched Layer (IV)

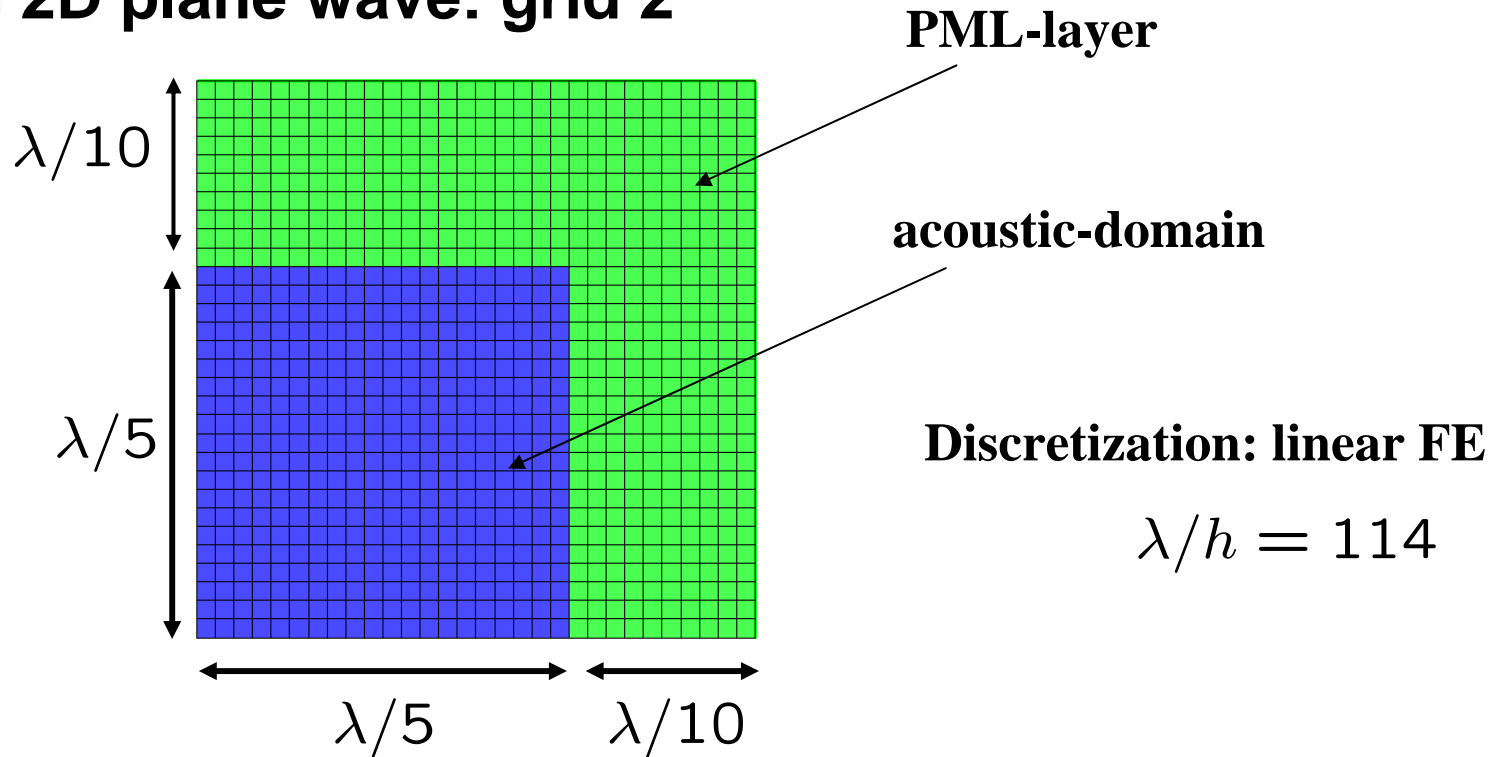
## 2D plane wave: grid 1



	ABC 1st order	PML const. ( $\sigma_0 = 14$ )	PML quadDist ( $\sigma_0 = 42$ )	PML inverseDist
L2-error	0.104	0.0072	0.0070	0.0040
rel. Error (0.5,0.5)	17%	0.63%	0.35%	0.34%

# Perfectly Matched Layer (V)

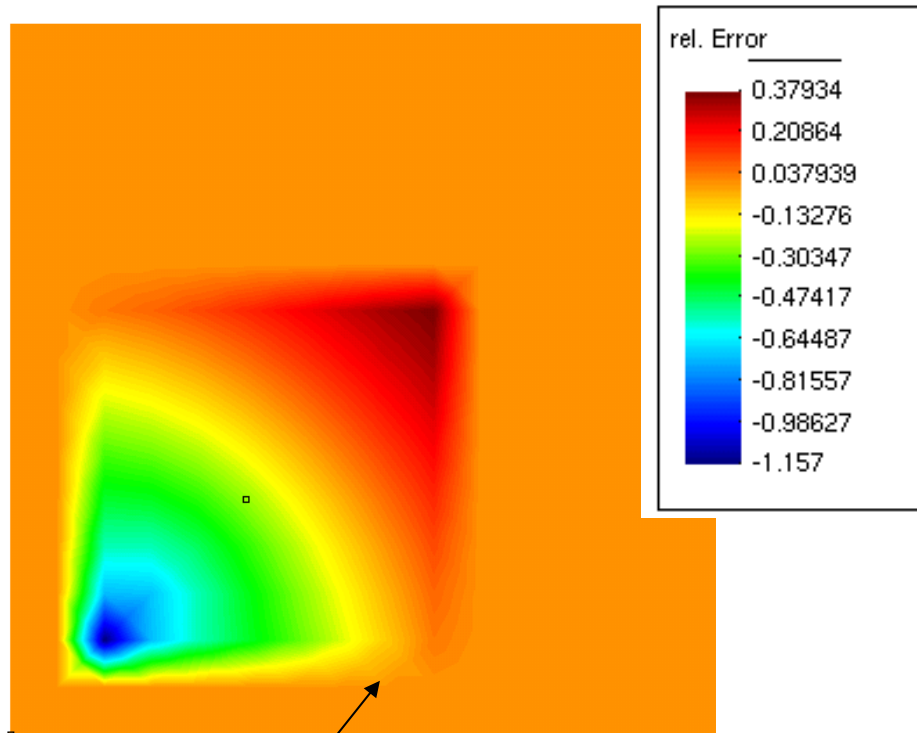
## 2D plane wave: grid 2



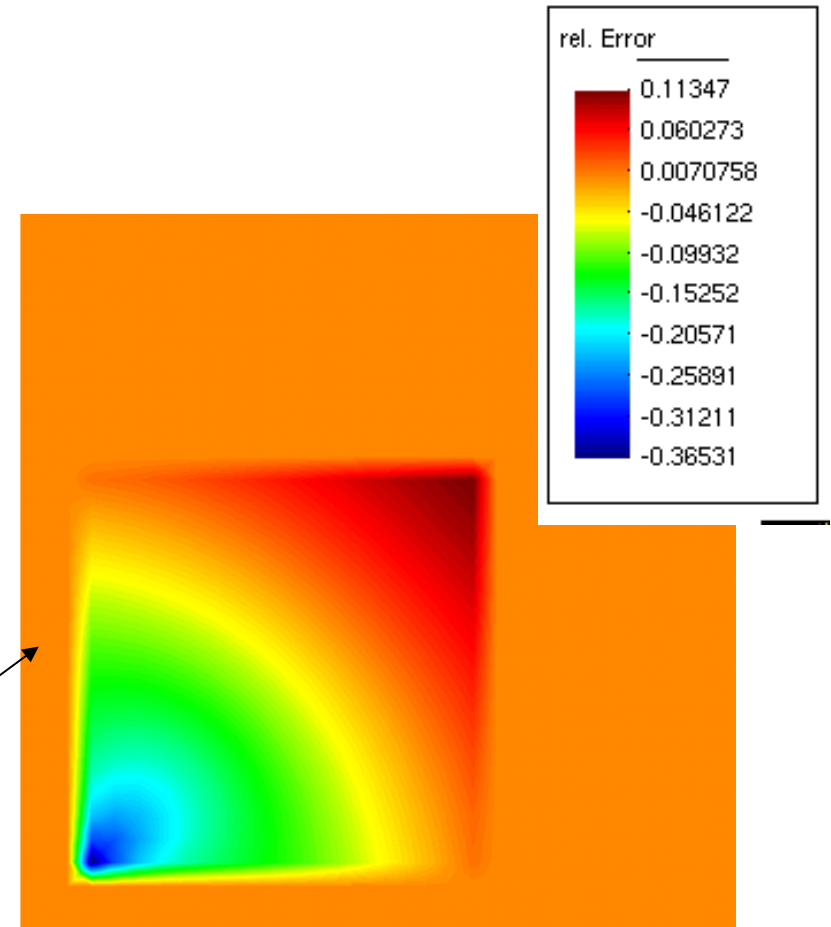
	ABC 1st order	PML const. ( $\sigma_{\max} = 14$ )	PML quadDist ( $\sigma_{\max} = 42$ )	PML inverseDist
L2-error	0.105	0.001613	0.001351	0.001193
rel. Error (0.5,0.5)	17%	0.22%	0.135%	0.11%

# Perfectly Matched Layer (VI)

## ❑ Error plots



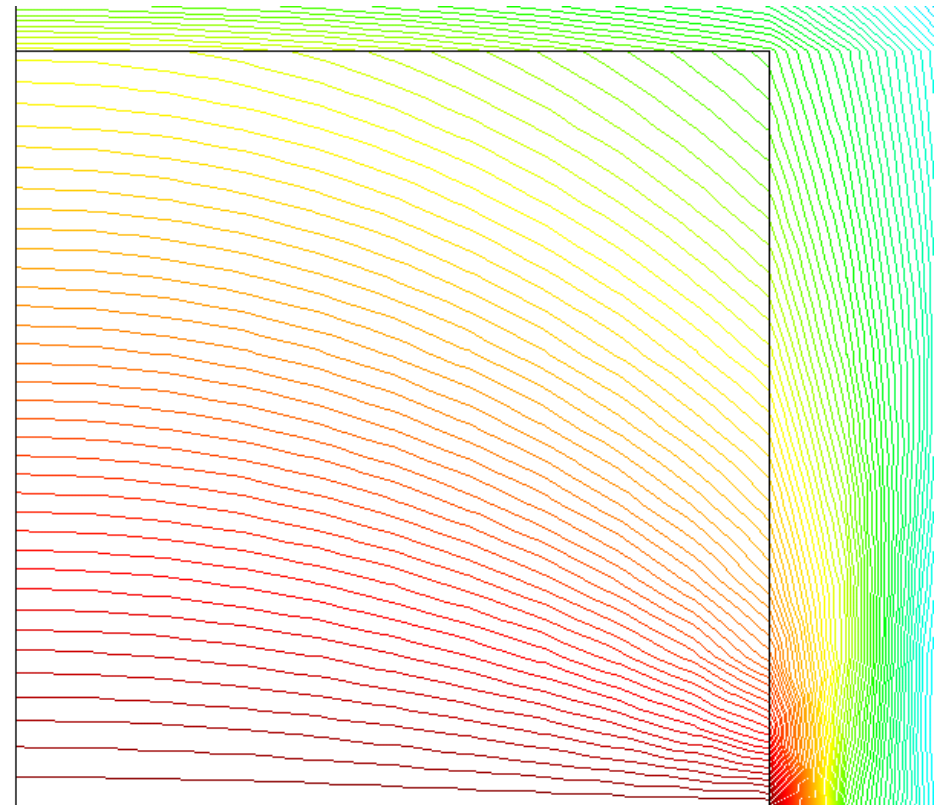
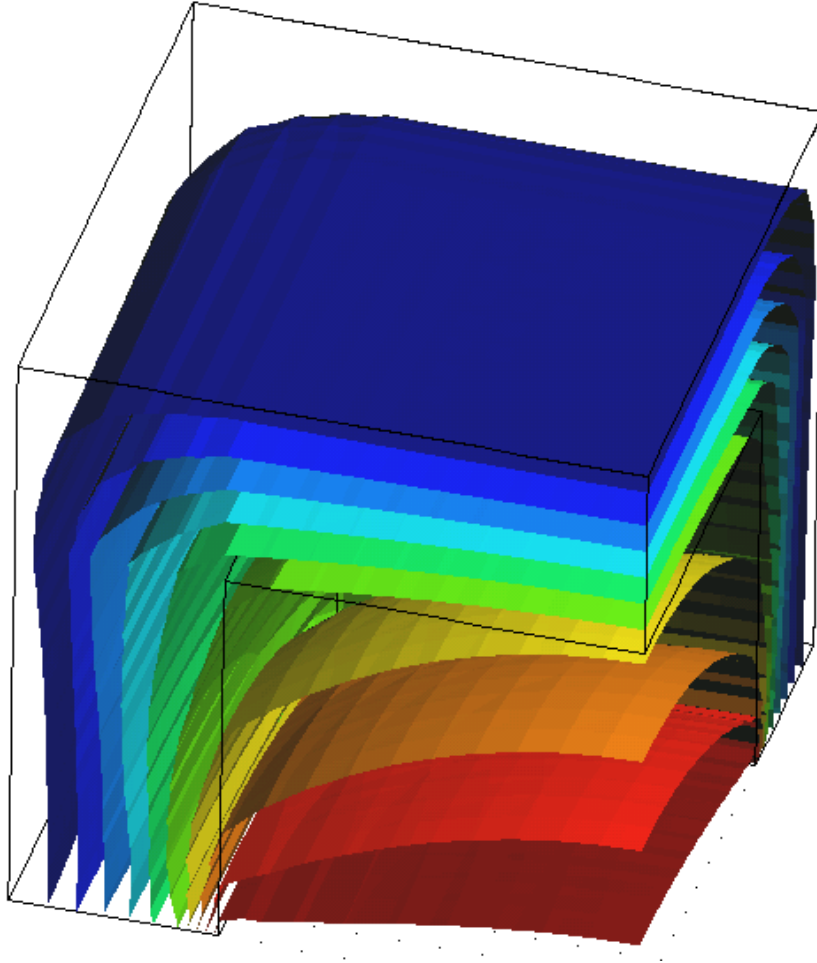
**Grid 1**



**Grid 2**

# Perfectly Matched Layer (VII)

## □ 3D example:





# Perfectly Matched Layer (VIII)

## □ Time domain ansatz:

$$\int \frac{\partial w}{\partial x_1} \frac{\gamma_{x_2} \gamma_{x_3}}{\gamma_{x_1}} \frac{\partial p}{\partial x_1} + \frac{\partial w}{\partial x_2} \frac{\gamma_{x_1} \gamma_{x_3}}{\gamma_{x_2}} \frac{\partial p}{\partial x_2} + \frac{\partial w}{\partial x_3} \frac{\gamma_{x_1} \gamma_{x_2}}{\gamma_{x_3}} \frac{\partial p}{\partial x_3} + \gamma(x_1) \gamma(x_2) \gamma(x_3) k^2 p = 0$$

$\frac{a_1}{s(s+b_1)}$ ;  $\frac{a_2}{s+b_2}$ ;  $\frac{sa_3}{s+b_3}$

$\frac{a_1 s}{s(s+b_1)} \frac{1}{s}$

$a_i e^{-b_i t}$

$c_1 s^2$ ;  $c_2 s$ ;  $c_3$ ;  $\frac{c_4}{s}$

$s \dots$  Laplace variable

**Convolution:**  $\psi(x, t) = a_i e^{-b_i t} * \mathcal{L}(p(x, t))$

$$\psi(x, t) = e^{-b_i(t-t_1)} \psi(x, t_1) + a e^{-bt} \int_{t_1}^t e^{b\tau} \mathcal{L}(p(x, \tau)) d\tau$$

# Further Cooperations (I)

## □ G. Of:

- Paper on *Fast Boundary Element Methods for Electrostatic Field Computations*

## □ FE/BE for Maxwell (eddy current case)

- Magnetic vector potential in solid parts (FE)

$$\mathbf{B} = \nabla \times \mathbf{A}$$

- Magnetic scalar potential in air-regions (BE)

$$\mathbf{H} = -\nabla \psi$$

We follow ideas of M. Kuhn and O. Steinbach

## □ M. Liebmann

- **Explicit time integration algorithm** for acoustic wave equation

# Further Cooperations (II)

## □ J. Kraus:

- Test of his AMG for large mechanical problems
- Adapt his AMG for Maxwell (edge element discretization)

## □ M. Nader:

- Control of flexible structures by piezoelectric patches

