

Mathematical Description and Modelling of Piezoelectric Systems

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Introduction

- Piezoelectric devices represent an important new group of actuators and sensors for active vibration control. This technology allows to construct spatially distributed devices.
- This fact requires special control techniques to improve the dynamical behavior of this kind of smart structures.
- A deeper insight in the mathematical structure of the models of smart structures will be given by the PCHD-approach.
- The controller design is based on a method for infinite dimensional Hamiltonian systems, which requires the collocation of sensors and actuators and therefore, certain distributed and/or integral quantities must be measured by means of the piezoelectric sensors.
- Some facts of modern control theory and of differential geometry are required

PCHD-Systems, ODE

Choice of a state space:

\mathcal{X} : q -dimensionale manifold with coordinates (x^α) , $\alpha = 1, \dots, q$.

Tangential- $\mathcal{T}(\mathcal{X})$, cotangential bundle $\mathcal{T}^*(\mathcal{X})$:

holonomic bases $\{\partial_\alpha\}$, $\{dx^\alpha\}$ with coordinates $(x^\alpha, \dot{x}^\alpha)$, $(x^\alpha, \dot{x}_\alpha)$.

Structure matrix: $J = -J^T$, dissipative effects: $R = R^T$, $R \geq 0$,

$$J; R : \mathcal{T}^*(\mathcal{X}) \rightarrow \mathcal{T}(\mathcal{X}) \quad \dot{x}^\alpha = \left(J^{\alpha\beta}(x) - R^{\alpha\beta}(x) \right) \dot{x}_\beta .$$

Ports: The input space $\mathcal{U} = \text{span}\{e_\varsigma\}$, a vector space with coordinates (u^ς) , $\varsigma = 1, \dots, m$ and a map B ,

$$B : \mathcal{U} \rightarrow \mathcal{T}(\mathcal{X}) \quad , \quad \dot{x}^\alpha = B_\varsigma^\alpha(x) u^\varsigma .$$

ODE (2)

The system

$$\dot{x}^\alpha = v_H^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta H + B_\zeta^\alpha u^\zeta ,$$

$$y_\zeta = B_\zeta^\alpha \partial_\alpha H$$

meets with $v_H = v_H^\alpha \partial_\alpha$,

$$v_H(H) = -\partial_\alpha (H) R^{\alpha\beta} \partial_\beta H + y_\zeta u^\zeta \leq y_\zeta u^\zeta$$

with the output space $\mathcal{Y} = \mathcal{U}^* = \text{span} \{e^\zeta\}$ with coordinates (y_ζ) and Hamiltonian $H \in C^\infty(\mathcal{X})$.

Exterior derivative:

$$\mathbb{R} \rightarrow C^\infty(\mathcal{X}) \xrightarrow{d} \wedge^1(\mathcal{T}^*(\mathcal{X})) \dots \xrightarrow{d} \wedge^q(\mathcal{T}^*(\mathcal{X})) \xrightarrow{d} \{0\} .$$

ODE (3)

Interior product:

$$\lrcorner : \mathcal{T}(\mathcal{X}) \times \wedge^r(\mathcal{T}^*(\mathcal{X})) \rightarrow \wedge^{r-1}(\mathcal{T}^*(\mathcal{X})) , \quad r \geq 0 .$$

Fact: v_H is no vector field. Choose a section σ of the bundle $\mathcal{U} \times \mathcal{X} \xrightarrow{\rho} \mathcal{X}$, then $(v_H^\alpha \circ \sigma) \partial_\alpha \in \Gamma(\mathcal{T}(\mathcal{X}))$ is met.

$$\begin{array}{ccc}
 \rho^*(\mathcal{T}(\mathcal{X})) & \xrightarrow{\tau^*(\rho)} & \mathcal{T}(\mathcal{X}) & & (x^\alpha, u^\varsigma, \dot{x}^\alpha) & \xrightarrow{\tau^*(\rho)} & (x^\alpha, \dot{x}^\alpha) \\
 \downarrow \rho^*(\tau) & & \downarrow \tau & & \uparrow v_H(x, u) & & v^* \uparrow v_H \circ g(x) \\
 \mathcal{U} \times \mathcal{X} & \xrightarrow{\rho} & \mathcal{X} & & (x^\alpha, u^\varsigma) & \xleftarrow{g(x)} & (x^\alpha)
 \end{array}$$

One gets $v_H \in \Gamma(\rho^*(\tau))$ with

$$\rho^*(\mathcal{T}(\mathcal{X})) \xrightarrow{\rho^*(\tau)} \mathcal{U} \times \mathcal{X} .$$

Coordinate Transformations

The structure of a PCHD-system is preserved by transformations of the type

$$\begin{aligned}\bar{x}^{\bar{\alpha}} &= \varphi^{\bar{\alpha}}(x) \\ \bar{u}^{\bar{s}} &= M_{\bar{\zeta}}^{\bar{s}}(x) (u^s + f^s(x)) \\ \bar{y}_{\bar{\zeta}} &= \bar{M}_{\bar{\zeta}}^s(x) (y_{\zeta} + \partial_{\alpha} H_f B_{\zeta}^{\alpha}) , \quad M_{\bar{\sigma}}^{\bar{s}} \bar{M}_{\bar{\zeta}}^{\sigma} = \delta_{\bar{\zeta}}^{\bar{s}} ,\end{aligned}$$

provided that one finds a function $H_f \in C^{\infty}(\mathcal{X})$ such that

$$\left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_{\beta} H_f + B_{\zeta}^{\alpha} f^{\zeta} = 0 .$$

Remark: For $f^{\zeta} = 0$ one chooses $H_f = 0$.

C.trans. (2)

Further relations

$$\begin{aligned}\bar{H} &= (H + H_f) \circ \varphi^{-1} \\ \bar{J}^{\bar{\alpha}\bar{\beta}} &= \left(\partial_{\alpha} \varphi^{\bar{\alpha}} J^{\alpha\beta} \partial_{\beta} \varphi^{\bar{\beta}} \right) \circ \varphi^{-1} \\ \bar{R}^{\bar{\alpha}\bar{\beta}} &= \left(\partial_{\alpha} \varphi^{\bar{\alpha}} R^{\alpha\beta} \partial_{\beta} \varphi^{\bar{\beta}} \right) \circ \varphi^{-1} \\ \bar{B}_{\bar{\zeta}}^{\bar{\alpha}} &= \left(\partial_{\alpha} \varphi^{\bar{\alpha}} B_{\zeta}^{\alpha} \bar{M}_{\bar{\zeta}}^{\zeta} \right) \circ \varphi^{-1} .\end{aligned}$$

Remark 1: The transformation for y, u is affine, therefore we get

$$y_{\zeta} u^{\zeta} \neq \bar{y}_{\bar{\zeta}} \bar{u}^{\bar{\zeta}} .$$

Remark 2: A function H_f , which meets the PDE with $f^{\zeta} = 0$, does not change the equations.

An Alternative

If there exist functions $H_\varsigma(x) \in C^\infty(\mathcal{X})$, such that

$$B_\sigma^\alpha = -J^{\alpha\beta} \partial_\beta H_\varsigma, \quad R^{\alpha\beta} \partial_\beta H_\varsigma = 0, \quad \partial_\beta (H_\varsigma) J^{\alpha\beta} \partial_\beta H_\varsigma = 0$$

is met, then one can rewrite the system as

$$\begin{aligned} \dot{x}^\alpha &= v_H^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta (H - H_\varsigma u^\varsigma), \\ y_\varsigma &= v_H (H_\varsigma). \end{aligned}$$

Remark: Often one chooses the output $Y_\varsigma = H_\varsigma$ instead of y_ς .
Furthermore,

$$y_\varsigma = \frac{d}{dt} Y_\varsigma$$

is met along a solution of the system.

D-Control

Damping injection $\mathbb{R}^{m \times m} \ni D \geq 0$:

$$\bar{x}^\alpha = x^\alpha$$

$$\bar{u}^\varsigma = D^{\varsigma\tau} y_\tau + u^\varsigma = D^{\varsigma\tau} B_\varsigma^\alpha \partial_\alpha H + u^\varsigma$$

$$\bar{y}_\varsigma = y_\varsigma$$

One derives the PCHD-system

$$\begin{aligned} \dot{x}^\alpha &= \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta H + B_\varsigma^\alpha \left(-D^{\varsigma\tau} y_\tau + \bar{u}^\varsigma \right) \\ &= \left(J^{\alpha\beta} - R^{\alpha\beta} - B_\varsigma^\alpha D^{\varsigma\tau} B_\tau^\beta \right) \partial_\beta H + B_\varsigma^\alpha \bar{u}^\varsigma, \end{aligned}$$

which meets

$$v_H(H) = -\partial_\alpha (H) \left(R^{\alpha\beta} + B_\varsigma^\alpha D^{\varsigma\tau} B_\tau^\beta \right) \partial_\beta H + y_\varsigma \bar{u}^\varsigma \leq y_\varsigma \bar{u}^\varsigma .$$

P/I-Regler

Choose the controller

$$\begin{aligned}\dot{\tilde{x}}^s &= \tilde{u}^s \\ \tilde{y}_\varsigma &= \partial_\varsigma \tilde{H} = P_{\varsigma\tau} \tilde{x}^\tau\end{aligned}$$

which is a PCHD system with $\tilde{J} = 0$, $\tilde{R} = 0$, $\tilde{H}(\tilde{x}) = \frac{1}{2} \tilde{x}^s P_{\varsigma\tau} \tilde{x}^\tau$,
 $\mathbb{R}^{m \times m} \ni P \geq 0$,

Connect the system

$$\begin{aligned}\dot{x}^\alpha &= \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta H + B_\varsigma^\alpha u^\varsigma \\ y_\varsigma &= B_\varsigma^\alpha \partial_\alpha H\end{aligned}$$

with the controller using the interconnection

$$u^s = -\delta^{s\tau} \tilde{y}_\tau + v^s, \quad \tilde{u}^s = \delta^{s\tau} y_\tau.$$

P/I (2)

$$\begin{aligned}\dot{x}^\alpha &= J^{\alpha\beta} \partial_\beta \left(H + \tilde{H} \right) - B_\tau^\alpha \delta^{\tau\varsigma} \partial_\varsigma \left(H + \tilde{H} \right) - R^{\alpha\beta} \partial_\beta \left(H + \tilde{H} \right) \\ \dot{\tilde{x}}^\varsigma &= \delta^{\varsigma\tau} B_\tau^\alpha \partial_\alpha \left(H + \tilde{H} \right)\end{aligned}$$

The transformation

$$\begin{aligned}\bar{x}^\alpha &= x^\alpha \\ \bar{\tilde{x}}^\varsigma &= \tilde{x}^\varsigma - \delta^{\varsigma\tau} Y_\tau(x) \\ \bar{\tilde{H}} &= \tilde{H}(\bar{\tilde{x}} + Y)\end{aligned}$$

leads to a lengthy PCHD-system.

Assumption: If relation $\partial_\alpha (Y_\varsigma) J^{\alpha\beta} \partial_\beta H = y_\varsigma = B_\varsigma^\alpha \partial_\alpha H$ and

$$R \partial_\beta (H) \partial_\alpha Y_\varsigma = B_\nu^\alpha \partial_\alpha Y_\varsigma = \partial_\alpha (Y_\varsigma) J^{\alpha\beta} \partial_\beta Y_\tau = 0$$

P/I (3)

are met, then one gets

$$\dot{\tilde{x}}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta H - B_\zeta^\alpha P^{\zeta\tau} \left(\tilde{x}^\tau + \delta^{\zeta\tau} Y_\tau \right) + B_\zeta^\alpha v^\zeta$$

$$\dot{\tilde{x}}^{\bar{s}} = 0$$

or

$$\dot{\tilde{x}}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta \left(H + \left(\tilde{x}^\tau + \delta^{\zeta\tau} Y_\tau \right) \frac{P^{\zeta\tau}}{2} \left(\tilde{x}^\tau + \delta^{\zeta\tau} Y_\tau \right) \right) + B_\zeta^\alpha v^\zeta .$$

H_2 -Control

Find a control law, such that the objective functional

$$\frac{1}{2} \int_0^{\infty} (y_s D^{s\tau} y_\tau + u^s \bar{D}_{s\tau} u^\tau) dt$$

with $D^{s\chi} \bar{D}_{\chi\tau} = \delta_\tau^s$ is minimized.

The HJB-inequality for this problem is

$$\inf_u (2v_H(V) + y_s D^{s\tau} y_\tau + u^s \bar{D}_{s\tau} u^\tau) \leq 0 .$$

Provided that H is a positive definite function then the choice

$$V = H$$

leads to

H_2 -Control (2)x

$$\inf_u \left(2\partial_\alpha (H) R^{\alpha\beta} \partial_\beta H + 2y_\varsigma u^\varsigma + y_\varsigma D^{s\tau} y_\tau + u^s \bar{D}_{s\tau} u^\tau \right) \leq 0$$
$$-2\partial_\alpha (H) R^{\alpha\beta} \partial_\beta H \leq 0$$

with the optimal control law

$$y_\varsigma = -\bar{D}_{s\tau} u^\tau, \quad u^s = -D^{s\tau} y_\tau.$$

H_∞ -Control

The system is given by

$$\dot{x}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta \left(H - H_\varsigma u^\varsigma - \hat{H}_\varsigma \hat{u}^\varsigma \right)$$

$$y_\varsigma = \partial_\alpha (H_\varsigma) J^{\alpha\beta} \partial_\beta H$$

$$\hat{y}_\varsigma = \partial_\alpha \left(\hat{H}_\varsigma \right) J^{\alpha\beta} \partial_\beta H ,$$

with $K \in \mathbb{R}^{qm}$, where u is the control and \hat{u} is the disturbance input.

Find a control law, such that the objective functional

$$\frac{1}{2} \int_0^\infty \left(\lambda^2 y_\varsigma \delta^{\varsigma\tau} y_\tau + u^\varsigma \delta_{\varsigma\tau} u^\tau - \gamma^2 \hat{u}^\varsigma \delta_{\varsigma\tau} \hat{u}^\tau \right) dt$$

is minimized with respect to u and maximized with respect to \hat{u} .

H_∞ -Control (2)

The HJBI-inequality for this problem is

$$\inf_u \sup_{\hat{u}} \left(2v_H(V) + \lambda^2 y_\varsigma \delta^{\varsigma\tau} y_\tau + u^\varsigma \delta_{\varsigma\tau} u^\tau - \gamma^2 \hat{u}^\varsigma \delta_{\varsigma\tau} \hat{u}^\tau \right) \leq 0 .$$

Provided that H is a positive definite function, then the choice $V = H$ leads to

$$\begin{aligned} \inf_u \sup_{\hat{u}} \left(2\partial_\alpha(H) R^{\alpha\beta} \partial_\beta H + 2y_\varsigma u^\varsigma + 2\hat{y}_\varsigma \hat{u}^\varsigma \right. \\ \left. + \lambda^2 y_\varsigma \delta^{\varsigma\tau} y_\tau + u^\varsigma \delta_{\varsigma\tau} u^\tau - \gamma^2 \hat{u}^\varsigma \delta_{\varsigma\tau} \hat{u}^\tau \right) &\leq 0 \\ -2\partial_\alpha(H) R^{\alpha\beta} \partial_\beta H + (\lambda^2 - 1) y_\varsigma \delta^{\varsigma\tau} y_\tau + \frac{1}{\gamma^2} \hat{y}_\varsigma \delta^{\varsigma\tau} \hat{y}_\tau &\leq 0 \end{aligned}$$

with the optimal choice

H_∞ -Control (3)

$$\gamma^2 \hat{u}^s \delta_{s\tau} = \hat{y}_\tau, \quad y_s = -\delta_{s\tau} u^\tau, \quad u^s = -\delta^{s\tau} y_\tau.$$

In the case $H_s = \hat{H}_s$ the condition simplifies to

$$-2\partial_\alpha (H) R^{\alpha\beta} \partial_\beta H + \left(\lambda^2 - 1 + \frac{1}{\gamma^2} \right) y_s \delta^{s\tau} y_\tau \leq 0$$

E.g. one chooses

$$\lambda^2 \leq \frac{\gamma^2 - 1}{\gamma^2}.$$

PCHD-Systeme, PDE

Choice of a state space:

\mathcal{B} an orientable smooth p -dimensional manifold with coordinates (X^i) , $i = 1, \dots, p$.

A compact p -dimensional manifold $\mathcal{D} \subset \mathcal{B}$ with boundary $\partial\mathcal{D}$ and volume form dX .

Inclusion map: $i : \partial\mathcal{D} \rightarrow \mathcal{D}$ with coordinates $(\bar{X}^{\bar{i}})$, $\bar{i} = 1, \dots, p - 1$ for $\partial\mathcal{D}$ and volume form $d\bar{X}$.

Bundle: $\mathcal{X} \xrightarrow{\pi} \mathcal{D}$ with coordinates (X^i, x^α) , $\alpha = 1, \dots, q$.

A section $\sigma \in \Gamma(\mathcal{X})$,

$$\pi \circ \sigma = \text{id}_{\mathcal{D}}, \quad \pi(X^i, x^\alpha) = (X^i)$$

represents the state of a distributed system.

PDE (2)

The first jet $j(\sigma)$ of σ , the functions σ^α and $\partial_i \sigma^\alpha$, is a section of the $J(\mathcal{X}) \xrightarrow{\pi^1} \mathcal{D}$ with the first jet-manifold $J(\mathcal{X})$, or $J(\pi)$, of \mathcal{X} . We use the adapted coordinates $(X^i, x^\alpha, x_{1_i}^\alpha)$.

Analogously one defines the n -th order jet $j^n(\sigma)$ of σ with $\partial_I \sigma^\alpha$, $\#I \leq n$.

The index $I = i_1, \dots, i_p$ is an ordered multi-index with $\#I = \sum_{j=1}^p i_j$,

which meets $I + J = i_1 + j_1, \dots, i_p + j_p$ and $1_i = i_1, \dots, i_j, \dots, i_p$, $i_j = \delta_j^i$ as well as

$$\partial_I = (\partial_1)^{i_1} \cdots (\partial_p)^{i_p} .$$

The coordinates of $J^n(\mathcal{X})$ are denoted by (X^i, x_I^α) , $0 \leq \#I \leq n$.

PDE (3)

With the projections

$$\pi_m^n (X^i, x^\alpha, x_I^\alpha) = (X^i, x^\alpha, x_J^\alpha) , \quad 0 \leq \#I \leq n , \quad 0 \leq \#J \leq m , \quad m < n$$

one derives the bundles

$$J^n (\mathcal{X}) \xrightarrow{\pi_m^n} J^m (\mathcal{X}) ,$$

with the identity $J^0 (\mathcal{X}) = \mathcal{X}$.

With the projection

$$\pi_m^n (X^i, x^\alpha, x_I^\alpha) = (X^i, x^\alpha)$$

one gets

$$J^n (\mathcal{X}) \xrightarrow{\pi^n} \mathcal{D} .$$

PDE (4)

The total derivative d_i with respect to X^i ,
 $d_i : C^\infty (J^n (\mathcal{X})) \rightarrow C^\infty (J^{n+1} (\mathcal{X}))$,

$$d_i = \partial_i + x_{I+1_i}^\alpha \partial_\alpha^I, \quad \partial_\alpha^I = \partial_{x_I^\alpha}.$$

meets

$$\partial_i (f \circ j^n (\sigma)) = (d_i f) \circ j^{n+1} (\sigma)$$

with $f \in C^\infty (J^n (\mathcal{X}))$, $\sigma \in \Gamma (\mathcal{X})$.

Remark: A section $\gamma \in \Gamma (J (\pi))$ does not necessarily meet $j (\sigma) = \gamma$ with $\sigma \in \Gamma (\pi)$, since the integrability conditions

$$\gamma_I^\alpha = \partial_I \gamma^\alpha$$

must be met.

PDE (5)

A section $\sigma \in \Gamma(\pi)$ defines a state. Obviously, σ fixes $j(\sigma)$.

Let us choose a section $\gamma \in \Gamma(\pi^1)$ with $j(\sigma) = \gamma$, and a section ϑ of $i^*(\pi) : i^*(\mathcal{X}) \xrightarrow{\pi|_{\partial\mathcal{D}}} \partial\mathcal{D}$.

Obviously, the state follows from

$$\sigma = \pi_0^1 \circ \gamma,$$

where the functions σ^α are solutions of the PDE

$$\partial_i \sigma^\alpha = \gamma_{1_i}^\alpha$$

with the boundary conditions given by ϑ .

PDE (6)

This is only possible for distributed parameter systems (PDEs) !

Ideal rod with Hamiltonian density $H = \frac{(x^2)^2}{2\rho} + \frac{E(x_{1_1}^1)^2}{2}$:

$$\dot{x}^1 = \frac{1}{\rho} x^2, \quad \dot{x}^2 = E x_{2_1}^1.$$

Die Lie-Bäcklund Transformation

$$\bar{x}^1 = x_{1_1}^1, \quad \bar{x}^2 = x^2$$

leads to

$$\dot{\bar{x}}^1 = \frac{1}{\rho} \bar{x}_{1_1}^2, \quad \dot{\bar{x}}^2 = E \bar{x}_{1_1}^1, \quad \bar{H} = \frac{1}{2\rho} (\bar{x}^2)^2 + \frac{E}{2} (\bar{x}^1)^2.$$

PDE (7)

Telegraphers equation with Hamiltonian density

$$H = \frac{1}{2C} (x^1)^2 + \frac{1}{2L} (x^2)^2$$

and

$$\dot{x}^1 = -\frac{1}{L} x_{1_1}^2, \quad \dot{x}^2 = -\frac{1}{C} x_{1_1}^1.$$

Remark: We confine ourselves to the case, where a state is defined by $\sigma \in \Gamma(\pi)$.

PDE (8)

Given the bundle $\mathcal{X} \xrightarrow{\pi} \mathcal{D}$ one gets several important bundles by standard constructions:

The tangent bundles $\mathcal{T}(\mathcal{X})$, $\mathcal{T}(\mathcal{D})$,
the cotangent bundles $\mathcal{T}^*(\mathcal{X})$, $\mathcal{T}^*(\mathcal{D})$.

The vertical tangential bundle of \mathcal{X} ,

$$\mathcal{V}(\mathcal{X}) = \ker(\pi_*) \subset \mathcal{T}(\mathcal{X}) ,$$

and the horizontal cotangent bundle

$$\mathcal{H}^*(\mathcal{X}) = \pi^*(\mathcal{T}^*(\mathcal{D})) \subset \mathcal{T}^*(\mathcal{X}) ,$$

which annuls $\mathcal{V}(\mathcal{X})$, or

$$\mathcal{V}(\mathcal{X}) \rfloor \mathcal{H}^*(\mathcal{X}) = \{0\} .$$

PDE (9)

Given these vector bundles one gets the further vector bundles

$$\wedge_r^0 (\mathcal{T}^* (\mathcal{X})) = \wedge_r (\mathcal{H}^* (\mathcal{X})) , \quad r \leq p$$

and

$$\wedge_p^1 (\mathcal{T}^* (\mathcal{X})) = (\mathcal{T}^* (\mathcal{X})) \wedge (\wedge_p (\mathcal{H}^* (\mathcal{X}))) ,$$

with

$$\mathcal{V} (\mathcal{X}) \rfloor \wedge_r^1 (\mathcal{T}^* (\mathcal{X})) = \wedge_r^0 (\mathcal{T}^* (\mathcal{X})) .$$

The interior product

$$\rfloor : \mathcal{V} (\mathcal{X}) \times \wedge_p^1 (\mathcal{T}^* (\mathcal{X})) \rightarrow \wedge_p^0 (\mathcal{T}^* (\mathcal{X})) , \quad r = \dot{x}^\alpha \dot{r}_\alpha$$

replaces the canonical product of the lumped parameter case.

(X^i, x^α, r) , $(X^i, x^\alpha, \dot{r}_\alpha)$ are coordinates for $\wedge_p^0 (\mathcal{T}^* (\mathcal{X}))$,
 $\wedge_p^1 (\mathcal{T}^* (\mathcal{X}))$.

PDE (10)

The total derivative d_i and the horizontal exterior derivative d_h are connected by

$$d_h = dX^i \wedge d_i ,$$

or by

$$j^{n+1}(\sigma)^*(d_h \omega) = d(j^n(\sigma)^*(\omega))$$

is met for all $\sigma \in \Gamma(\mathcal{X})$, $\omega \in \Gamma(\wedge \mathcal{T}^*(J^n(\mathcal{X})))$.

Remark: The sequence

$$\mathbb{R} \rightarrow C^\infty(\mathcal{X}) \xrightarrow{d_h} \wedge_1^0(\mathcal{T}^*(\mathcal{X})) \dots \xrightarrow{d_h} \wedge_p^0(\mathcal{T}^*(\mathcal{X})) \xrightarrow{d_h} \{0\}$$

is exact.

PDE (11)

Consider d_h as a map

$$d_h : \pi^{n,*} (\wedge_r (\mathcal{H}^* (\mathcal{X}))) \rightarrow \pi^{n+1,*} (\wedge_{r+1} (\mathcal{H}^* (\mathcal{X}))) ,$$

then one derives a version of Stokes's Theorem, adapted to bundles:

$$\int_{\partial \mathcal{D}} j^n (\sigma)^* (\omega) = \int_{\mathcal{D}} j^{n+1} (\sigma)^* (d_h \omega)$$

is met for all $\sigma \in \Gamma (\mathcal{X})$, $\omega \in \Gamma (\pi^{n,*} (\wedge_{p-1} (\mathcal{T}^* (\mathcal{D}))))$.

The Hamiltonian of the lumped parameter case is replaced by the Hamiltonian density

$$HdX \in \pi_0^{1,*} (\wedge_p^0 (\mathcal{T}^* (\mathcal{D}))) .$$

PDE (12)

The exterior derivative of

$$\begin{aligned}
 d(HdX) &= \partial_\alpha H dx^\alpha \wedge dX + \partial_\alpha^i H dx_{1_i}^\alpha \wedge dX \\
 &= \partial_\alpha H dx^\alpha \wedge dX + \partial_\alpha^i H d_i (dx^\alpha \wedge dX) \\
 &= \underbrace{\left((\partial_\alpha - d_i \partial_\alpha^i) H \right)}_{\delta_\alpha} dx^\alpha \wedge dX + d_h (\partial_\alpha^i H \partial_i \rfloor dx^\alpha \wedge dX)
 \end{aligned}$$

induces two new maps: The variational derivative δ ,

$$\delta : \pi_0^{1,*} (\wedge_p^0 (\mathcal{T}^* (\mathcal{X}))) \rightarrow \pi_0^{2,*} (\wedge_p^1 (\mathcal{T}^* (\mathcal{X}))) .$$

Using the coordinates $(X^i, x^\alpha, \dot{r}_\alpha)$ for $\wedge_p^1 (\mathcal{T}^* (\mathcal{X}))$ we get

$$\dot{r}_\alpha = \delta_\alpha (H) \quad \text{with} \quad \delta_\alpha = \partial_\alpha + \sum_I (-1)^{\#I} d_I \partial_\alpha^I .$$

PDE (13)

Remark: The sequence

$$\Lambda_{p-1}^0(\mathcal{T}^*(\mathcal{X})) \xrightarrow{d_h} \Lambda_p^0(\mathcal{T}^*(\mathcal{X})) \xrightarrow{\delta} \Lambda_p^1(\mathcal{T}^*(\mathcal{X}))$$

is exact.

Now, on the boundary $\partial\mathcal{D}$ the bundle

$$\Lambda_{p-1}^1(\mathcal{T}^*(i^*(\mathcal{X})))$$

with local coordinates $(\hat{X}^i, \hat{x}^\alpha, \hat{r}_\alpha)$ takes over the function of $\Lambda_p^1(\mathcal{T}^*(\mathcal{X}))$.

PDE (14)

From

$$i^* (\partial_\alpha^i H \partial_i] dx^\alpha \wedge dX) = i^* (\partial_\alpha^i H) \gamma_i dx^\alpha \wedge d\bar{X} , \quad \gamma_i \in C^\infty (\partial\mathcal{D})$$

one gets the second map

$$\zeta : \pi_0^{1,*} (\wedge_p^0 (\mathcal{T}^* (\mathcal{X}))) \rightarrow \pi_0^{1,*} (\wedge_{p-1}^1 \mathcal{T}^* (i^* (\mathcal{X}))) ,$$

given in coordinates by

$$\hat{r}_\alpha = i^* (\zeta_\alpha (H)) , \quad \zeta_\alpha = \gamma_i \partial_\alpha^i .$$

Fact: The exterior derivative of the Hamiltonian density splits into the two maps δ , ζ in a natural manner.

PDE (15)

Given a skew symmetric map

$$J : \pi_0^{2,*} (\wedge_p^1 (\mathcal{T}^* (\mathcal{X}))) \rightarrow \pi_0^{2,*} (\mathcal{V} (\mathcal{X}))$$

or in coordinates

$$\dot{x}^\alpha = J^{\alpha\beta} \dot{r}_\beta, \quad J^{\alpha\beta} \in C^\infty (J^2 (\mathcal{X}))$$

one derives the evolutionary Hamiltonian equations as

$$\dot{x}^\alpha = v^\alpha, \quad v^\alpha = J^{\alpha\beta} \delta_\beta (H)$$

with the Hamiltonian operator $v \in \pi_0^{2,*} (\mathcal{V} (\mathcal{E}))$.

The change of $\int_{\mathcal{D}} H dX$ along solutions of the system is given by

$$\int_{\mathcal{D}} j(v)(H dX) = \int_{\mathcal{D}} \underbrace{\delta_\alpha (H) J^{\alpha\beta} \delta_\beta (H)}_{=0} dX + \int_{\partial\mathcal{D}} v^\alpha (\partial_\alpha^i H) \gamma_i d\bar{X}.$$

PDE (16)

Remark 1: If suitable boundary conditions are chosen, such that

$$v^\alpha (\partial_\alpha^i H) \gamma_i = 0$$

is met, then $\int_{\mathcal{D}} H dX$ is an invariant.

Remark 2: The interior product

$$\mathcal{V}(i^*(\mathcal{X})) \times \wedge_{p-1}^1 \mathcal{T}^*(i^*(\mathcal{X})) \rightarrow \wedge_{p-1}^0 \mathcal{T}^*(i^*(\mathcal{X}))$$

measure the flow of power over the boundary.

Remark 3: J can be replaced by skew symmetric differential operator,

$$J^{\alpha\beta} = J^{\alpha\beta I} d_I, \quad \#I \leq r, \quad d_I = (d_1)^{i_1} \circ \dots \circ (d_1)^{i_1}.$$

PDE (17)

The choice of a positive semi definite map

$$R : \pi_0^{2,*} (\wedge_p^1 (\mathcal{T}^* (\mathcal{X}))) \rightarrow \pi_0^{2,*} (\mathcal{V} (\mathcal{X}))$$

allows us to take dissipative effects into account. One gets

$$\dot{x}^\alpha = v^\alpha, \quad v^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta (H),$$

as well as

$$\int_{\mathcal{D}} j(v)(H) dX = - \int_{\mathcal{D}} \underbrace{\delta_\alpha(H) R^{\alpha\beta} \delta_\beta(H)}_{\geq 0} dX + \int_{\partial\mathcal{D}} v^\alpha (\partial_\alpha^i H) \gamma_i d\bar{X}.$$

Remark 1: Provided that suitable boundary conditions are chosen, then $\int_{\mathcal{D}} H dX$ is non-increasing along solutions.

Remark 2: One can also replace R by a differential operator.

PDE (18)

To introduce ports we choose the vector bundle \mathcal{U} as an input space

$$(\mathcal{U}, \rho, \mathcal{D}) \quad \text{with coordinates} \quad (X^i, u^\varsigma) \quad , \quad \varsigma = 1, \dots, m .$$

The output space is given by the vector bundle $(\mathcal{Y}, \rho^*, \mathcal{D})$, which is dual with respect to the product

$$\rho \times \rho^* \rightarrow \wedge_p (\mathcal{T}^* (\mathcal{D}))$$

and in coordinates given by $r = u^\varsigma y_\varsigma$, with coordinates (X^i, y_ς) for \mathcal{Y} .

Let us choose a linear map $B : \mathcal{U} \rightarrow \pi^{2,*} (\mathcal{V} (\mathcal{X}))$, then one derives the system

$$\dot{x}^\alpha = v_H^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta H + B_\varsigma^\alpha u^\varsigma$$

$$y_\varsigma = B_\varsigma^\alpha \delta_\alpha H ,$$

PDE (19)

as well as

$$\int_{\mathcal{D}} j(v)(H dX) = - \int_{\mathcal{D}} \underbrace{\delta_{\alpha}(H) R^{\alpha\beta} \delta_{\beta}(H)}_{\geq 0} dX + \int_{\mathcal{D}} y_{\zeta} u^{\zeta} dX$$
$$+ \int_{\partial\mathcal{D}} v^{\alpha} (\partial_{\alpha}^i H) \gamma_i d\bar{X} \leq \int_{\mathcal{D}} y_{\zeta} u^{\zeta} dX .$$

Remark 1: One can replace B by a differential operator.

Remark 2: Ports on the boundary can be introduced in a similar manner.

H. Ennsbrunner, K. Schlacher: *On the geometrical representation and interconnection of infinite dimensional port controlled Hamiltonian systems*. To appear in the proceedings of CDC-ECC, Sevilla, Spain 2005.

PDE (20)

An alternative approach: One chooses finite dimensional vector spaces \mathcal{U} , $\mathcal{Y} = \mathcal{U}^*$.

Given a linear map

$$B : \mathcal{U} \rightarrow \pi^{2,*}(\mathcal{V}(\mathcal{X}))$$

and its dual

$$B^* : \pi_0^{2,*}(\wedge_p^1(\mathcal{T}^*(\mathcal{X}))) \rightarrow \mathcal{Y},$$

then one derives the system

$$\dot{x}^\alpha = v_H^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta H + B_\zeta^\alpha u^\zeta$$

$$y_\zeta = \int_{\mathcal{D}} B_\zeta^\alpha \delta_\alpha H dX .$$

PDE (21)

An alternative: If there exists functions $H_\varsigma \in C^\infty(\mathcal{X})$, such that

$$B_\sigma^\alpha = -J^{\alpha\beta} \delta_\beta H_\varsigma, \quad R^{\alpha\beta} \delta_\beta H_\varsigma = 0, \quad \delta_\beta (H_\varsigma) J^{\alpha\beta} \delta_\beta H_\varsigma = 0$$

is met, then one can rewrite the system as

$$\begin{aligned} \dot{x}^\alpha &= v_H^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta (H - H_\varsigma u^\varsigma), \\ y_\varsigma &= v_H (H_\varsigma). \end{aligned}$$

Remark: Often one chooses the output $Y_\varsigma = H_\varsigma$ instead of y_ς .
Furthermore,

$$y_\varsigma = \frac{d}{dt} Y_\varsigma$$

is met along solutions of the system.

PDE (22)

Remark: If $H_\varsigma \in C^\infty (J(\mathcal{X}))$ is met, then the input map B is already a differential operator because of

$$J^{\alpha\beta} \delta_\beta (H_\varsigma u^\varsigma) = J^{\alpha\beta} \left(\partial_\alpha (H_\varsigma) u^\varsigma + \sum_I (-1)^{\#I} d_I \left(\partial_\alpha^I (H_\varsigma) u^\varsigma \right) \right),$$

where d_i is extended by $u_{I+1_i}^\varsigma \partial_\sigma^I$.

Coordinaten transformations, PDE

The structure of a PCHD system is invariant with respect to bundle isomorphism (ψ, φ) of the type

$$\begin{aligned}\bar{X}^{\bar{i}} &= \psi^{\bar{i}}(x) \\ \bar{x}^{\bar{\alpha}} &= \varphi^{\bar{\alpha}}(X, x) .\end{aligned}$$

One gets

$$\begin{aligned}\bar{H} &= H_0 \circ j(\psi, \varphi)^{-1} \\ \bar{J}^{\bar{\alpha}\bar{\beta}} &= \left(\partial_{\alpha} \varphi^{\bar{\alpha}} J^{\alpha\beta} \partial_{\beta} \varphi^{\bar{\beta}} \right) \circ j^2(\psi, \varphi)^{-1} \\ \bar{R}^{\bar{\alpha}\bar{\beta}} &= \left(\partial_{\alpha} \varphi^{\bar{\alpha}} R^{\alpha\beta} \partial_{\beta} \varphi^{\bar{\beta}} \right) \circ j^2(\psi, \varphi)^{-1} ,\end{aligned}$$

where $j(\psi, \varphi)$, $j^2(\psi, \varphi)$ denote the prolongations of (ψ, φ) to $J(\pi)$, $J^2(\pi)$.

K.trans. PDE (2)

Remark: E.g. $j(\psi, \varphi)$ is given by

$$\bar{x}_{1_i}^{\bar{\alpha}} \partial_i \psi^{\bar{i}} = d_i \varphi^{\bar{\alpha}} .$$

Input and output transformation according to

$$\begin{aligned} \bar{u}^{\bar{\varsigma}} &= M_{\bar{\varsigma}}^{\bar{\varsigma}} (u^{\varsigma} + f^{\varsigma}) \\ \bar{y}_{\bar{\varsigma}} &= \bar{M}_{\bar{\varsigma}}^{\varsigma} (y_{\varsigma} + \delta_{\alpha} (H_f) B_{\varsigma}^{\alpha}) , \quad M_{\bar{\sigma}}^{\bar{\varsigma}} \bar{M}_{\varsigma}^{\sigma} = \delta_{\bar{\varsigma}}^{\bar{\sigma}} \end{aligned}$$

with $M_{\bar{\varsigma}}^{\bar{\varsigma}}, f^{\varsigma} \in C^{\infty} (J^2 (\mathcal{X}))$, provided that there exist a function $H_f \in C^{\infty} (J^2 (\mathcal{X}))$, which meets

$$\left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_{\beta} H_f + B_{\varsigma}^{\alpha} f^{\varsigma} = 0 .$$

K.trans. PDE (3)

Remark: Take into account, that the kernel of δ is non-trivial.

The input matrix B transforms as

$$\bar{B}_{\bar{\zeta}}^{\bar{\alpha}} = (\partial_{\alpha} \varphi^{\bar{\alpha}} B_{\zeta}^{\alpha} \bar{M}_{\bar{\zeta}}^{\zeta}) \circ j^2 (\psi, \varphi)^{-1} .$$

Remark 1: Inputs and outputs are transformed in an affine manner.

Remark 2: Given a solution H_f for $f = 0$, then the choice $H + H_f$ leads to the same evolutionary equations, but may change the boundary conditions.

D-Control, PDE

Damping injection: One connects the system

$$\begin{aligned}\dot{x}^\alpha &= v_H^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta H + B_\zeta^\alpha u^\zeta \\ y_\zeta &= B_\zeta^\alpha \delta_\alpha H ,\end{aligned}$$

with

$$u^\zeta = -\tilde{y}^\zeta + v^\zeta , \quad \tilde{u}_\zeta = y_\zeta , \quad \tilde{y}^\zeta = D^{\zeta\tau} \tilde{u}_\tau ,$$

$C^\infty(\mathcal{D})^{m \times m} \ni D \geq 0$ and derives

$$\begin{aligned}\dot{x}^\alpha &= \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta H + B_\zeta^\alpha \left(-D^{\zeta\tau} y_\tau + \bar{u}^\zeta \right) \\ &= \left(J^{\alpha\beta} - R^{\alpha\beta} - B_\zeta^\alpha D^{\zeta\tau} B_\tau^\beta \right) \delta_\beta H + B_\zeta^\alpha \bar{u}^\zeta .\end{aligned}$$

D, PDE (2)

Damping injection on the boundary: Let us introduce ports on $\partial\mathcal{D}$ such that

$$v^\alpha (\partial_\alpha^i H) \gamma_i = \hat{y}_{\hat{\zeta}} \hat{u}^{\hat{\zeta}},$$

$\hat{\zeta} = 1, \dots, \hat{m}$ is met, then the choice

$$\hat{u}^{\hat{\zeta}} = -\hat{D}^{\hat{\zeta}\hat{\tau}} \hat{y}_{\hat{\tau}}$$

with $C^\infty(\mathcal{D})^{\hat{m} \times \hat{m}} \ni D \geq 0$ leads to

$$\int_{\partial\mathcal{D}} v^\alpha (\partial_\alpha^i H) \gamma_i d\bar{X} = - \int_{\partial\mathcal{D}} \hat{y}_{\hat{\zeta}} \hat{D}^{\hat{\zeta}\hat{\tau}} \hat{y}_{\hat{\tau}} d\bar{X} \leq 0.$$

P/I-Control, PDE

Connect the system

$$\dot{x}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta H + B_\zeta^\alpha u^\zeta$$

$$y_\zeta = B_\zeta^\alpha \partial_\alpha H$$

by

$$u^\zeta = -\tilde{y}^\zeta + v^\zeta, \quad \tilde{u}_\zeta = y_\zeta$$

with the controller

$$\dot{\tilde{x}}^\zeta = \tilde{u}^\zeta$$

$$\tilde{y}_\zeta = \partial_\zeta \tilde{H} = \delta_\zeta \tilde{H} = P_{\zeta\tau} \tilde{x}^\tau$$

with $\tilde{J} = 0$, $\tilde{R} = 0$, $\tilde{H}(\tilde{x}) = \frac{1}{2} \tilde{x}^\zeta P_{\zeta\tau} \tilde{x}^\tau$, $C^\infty(\mathcal{D})^{m \times m} \ni P \geq 0$, then one gets

P/I, PDE (2)

$$\dot{x}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \delta_\beta H - B_\zeta^\alpha \partial^\zeta \tilde{H} + B_\zeta^\alpha v^\zeta$$

$$\dot{\tilde{x}}_\zeta = B_\zeta^\alpha \delta_\alpha H .$$

Provided that $J^{\alpha\beta} \delta_\beta (H) \partial_\alpha Y_\zeta = y_\zeta = B_\zeta^\alpha \delta_\alpha H$ and

$$R^{\alpha\beta} \delta_\beta (H) \partial_\alpha Y_\zeta = 0 , \quad B_v^\alpha \partial_\alpha Y_\zeta = 0 , \quad J^{\alpha\beta} \delta_\beta (H_\tau) \partial_\alpha Y_\zeta = 0$$

is met, then the transformation

$$\bar{x}^\alpha = x^\alpha$$

$$\bar{\tilde{x}}_\zeta = \tilde{x}_\zeta - Y_\zeta (X, x)$$

$$\bar{\tilde{H}} = \tilde{H} (\bar{\tilde{x}} + Y)$$

P/I, PDE (3)

leads to

$$\dot{\tilde{x}}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta (H+) - B_\zeta^\alpha P^{\zeta\tau} (\tilde{x}_\tau + Y_\tau) + B_\zeta^\alpha v^\zeta$$

$$\dot{\tilde{x}}_\zeta = 0$$

or

$$\dot{\tilde{x}}^\alpha = \left(J^{\alpha\beta} - R^{\alpha\beta} \right) \partial_\beta \left(H + (\tilde{x}_\zeta + Y_\zeta) \frac{P^{\zeta\tau}}{2} (\tilde{x}_\tau + Y_\tau) \right) + B_\zeta^\alpha v^\zeta .$$

Remark: P/I-design for a boundary control is analogous.

Etc. PDE

H_2 -Control and H_∞ -control are extensible to the PDE case.

Controller design with Casimirs:

A. Macchelli, A. van der Schaft, C. Melchiorri: *Control by interconnection for distributed port Hamiltonian systems*.

Proceedings: IFAC World Congress, Prague, 2005.

State feedback, simple or IDA-PBC, can be extended to the PDE case.

In certain cases the controller can be any passive system.

Open problem: A simple and straightforward stability proof is missing.

Summary PDE

The approach is based on

lumped parameter	distributed parameter
$H \in C(\mathcal{X})$	$HdX \in \Lambda_p^0(\mathcal{T}^*(\mathcal{D}))$
$d : C(\mathcal{X}) \rightarrow \mathcal{T}^*(\mathcal{X})$	$\delta : \Lambda_p^0(\mathcal{T}^*(\mathcal{X})) \rightarrow \Lambda_p^1(\mathcal{T}^*(\mathcal{X}))$ $\zeta : \Lambda_p^0(\mathcal{T}^*(\mathcal{X})) \rightarrow \Lambda_{p-1}^1 \mathcal{T}^*(i^*(\mathcal{X}))$
$J, R : \mathcal{T}^*(\mathcal{X}) \rightarrow \mathcal{T}(\mathcal{X})$	$J, R : \Lambda_p^0(\mathcal{T}^*(\mathcal{X})) \rightarrow \mathcal{V}(\mathcal{X})$
$v_H \in \Gamma(\mathcal{T}(\mathcal{X}))$	$v_H \in \Gamma(\mathcal{V}(\mathcal{X}))$
$B : \mathcal{U} \rightarrow \mathcal{T}(\mathcal{X})$	$B : (\mathcal{U}, \rho, \mathcal{D}) \rightarrow \mathcal{V}(\mathcal{X})$
$B^* : \mathcal{T}^*(\mathcal{X}) \rightarrow \mathcal{Y} = \mathcal{U}^*$	$B^* : \Lambda_p^1(\mathcal{T}^*(\mathcal{X})) \rightarrow \mathcal{Y} = \mathcal{U}^*$

Piezoelectric Systems

We consider the linear elastic and time invariant case only.

\mathcal{D} manifold of the independent spatial coordinates (X^i) , $i = 1, 2, 3$, which is the standard 3-dimensional Euclidean space.

The total manifold $(\mathcal{X}, \pi, \mathcal{D})$ is equipped with the local coordinates (X^i, x^χ) , $\chi = 1 \dots 6$ with $x = (u^\alpha, p_\alpha)$, $\alpha = 1, 2, 3$, u^α are the displacements, p_α are the generalized momenta.

We assume, that there exists an energy function e_E ,

$$\begin{aligned} d(e_E + E_\alpha D^\alpha) \wedge dX &= \left(\sigma^{\alpha\beta} d\varepsilon_{\alpha\beta} + E_\alpha dD^\alpha \right) \wedge dX \\ &= \left(\sigma^{\alpha\beta} d\varepsilon_{\alpha\beta} + d(E_\alpha D^\alpha) - D^\alpha dE_\alpha \right) \wedge dX \end{aligned}$$

with the stress

$$\sigma = \sigma^{\alpha\beta} \partial_\alpha \otimes \partial_\beta, \quad \sigma^{\alpha\beta} = \sigma^{\beta\alpha},$$

Piezo (2)

the strain

$$\varepsilon = \varepsilon_{\alpha\beta} dx^\alpha \otimes dx^\beta, \quad 2\varepsilon_{\alpha\beta} = u_{1_\beta}^\alpha + u_{1_\alpha}^\beta,$$

the electrical field strength $E = E_\alpha dX^\alpha$ and the electrical displacement $D = D^\alpha \partial_\alpha \rfloor dX$.

The linearized constitutive equations are

$$\sigma^{\alpha\beta} = C^{\alpha\beta\gamma\delta} \varepsilon_{\gamma\delta} - G^{\alpha\beta\gamma} E_\gamma$$

$$D^\alpha = G^{\beta\gamma\alpha} \varepsilon_{\beta\gamma} + F^{\alpha\beta} E_\beta,$$

$\beta, \gamma = 1, 2, 3$ with $C^{\alpha\beta\gamma\delta}, G^{\alpha\beta\gamma}, F^{\alpha\beta} \in C^\infty(\mathcal{D})$.

Piezo (3)

If the integrability conditions are $C^{\alpha\beta\gamma\delta} = C^{\beta\alpha\gamma\delta} = C^{\alpha\beta\delta\gamma} = C^{\gamma\delta\alpha\beta}$, $G^{\alpha\beta\gamma} = G^{\beta\alpha\gamma}$, $F^{\alpha\beta} = F^{\beta\alpha}$ are met, we get the density $e_E dX$,

$$e_E dX = \left(\frac{1}{2} \varepsilon_{\alpha\beta} C^{\alpha\beta\gamma\delta} \varepsilon_{\gamma\delta} - G^{\alpha\beta\gamma} E_\gamma \varepsilon_{\alpha\beta} - \frac{1}{2} F^{\alpha\beta} E_\alpha E_\beta \right) dX .$$

With the kinetic energy density $e_K dX$,

$$e_K dX = \frac{1}{2\rho} p_\alpha \delta^{\alpha\beta} p_\beta dX ,$$

with $\rho \in C^\infty(\mathcal{D})$, we derive the Hamiltonian density $H dX$ of the free system,

$$H dX = \left(e_k + \frac{1}{2} \varepsilon_{\alpha\beta} C^{\alpha\beta\gamma\delta} \varepsilon_{\gamma\delta} \right) dX .$$

Piezo (4)

If one chooses E_γ as the control input, then the Hamiltonian density of the plant is

$$\left(H - G^{\alpha\beta\gamma} \varepsilon_{\alpha\beta} E_\gamma \right) dX ,$$

and we derive the evolutionary equations as

$$\dot{u}^\alpha = \delta^\alpha H = \frac{1}{\rho} p_\alpha$$

$$\dot{p}_\alpha = -\delta_\alpha H = d_i \left(\varepsilon_{\gamma\delta} C^{\alpha i \gamma \delta} - G^{\alpha i \gamma} E_\gamma \right)$$

with J, R ,

$$J = \begin{bmatrix} 0 & I_{3 \times 3} \\ -I_{3 \times 3} & 0 \end{bmatrix} , \quad R = 0 .$$

Piezo (5)

The collocated output is

$$y^\gamma = d_i \left(\frac{1}{\rho} p_\alpha G^{\alpha i \gamma} \right) .$$

Of special interest is the case, where the electrical field strength E has a potential $U^\varsigma \Phi_\varsigma$, or

$$E = U^\varsigma d_h \Phi_\varsigma , \quad \Phi_\varsigma \in C^\infty (J^n (\mathcal{X}))$$

is met.

Let us choose the voltages U^ς , $\varsigma = 1, \dots, m$ as inputs, then the Hamiltonian density is given by

$$\left(H - G^{\alpha\beta\gamma} \varepsilon_{\alpha\beta} d_\gamma (\Phi_\varsigma) U^\varsigma \right) dX = (H - H_\varsigma U^\varsigma) dX .$$

Piezo (5)

Let the the Hamiltonian density be is given by

$$\left(H - H_\zeta U^\zeta - \hat{H}_\zeta \hat{d}^\zeta \right) dX$$

with the disturbance \hat{d}^ζ .

Actuator shaping: How must we design the actuator, such that it acts in the same manner on the structure like the disturbances?

Answer: The relation

$$\delta \left(\left(H_\tau a_\zeta^\tau - \hat{H}_\zeta \right) dX \right) = 0$$

must be met for $a_\zeta^\tau \in \mathbb{R}$. Furthermore, one has to add suitable boundary condition.

Conclusions

- PCHD-systems have turned out to be a very useful tool for the analysis and design in the ODE case.
- The extension of the approach to the PDE case is not unique at all.
- The presented approach works well for piezoelectric systems.
- Temperature effects lie outside the presented framework, but they can be taken into account by a nonlinear approach.
- Several control schemes like D- or PD-control can be adopted in a more or less straightforward manner, others like H_2 - or H_∞ -control can be extended under certain circumstances. Also state feedback design approaches like IDA-PBC need further investigations concerning the implementation.



Thank you for attending.